

# Stronger at the Broken Places:

## A Free-Energy Theory of Golden Repair in Fractured Solids and Social Networks

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### Abstract

A repaired object is usually assumed to be, at best, as good as it was before it broke. We report that this is false. We define the *Kintsugi coefficient*  $\kappa$ , the ratio of a specimen’s fracture toughness after a visible golden repair to its toughness when pristine, and show—across ceramics, engineering teams, and simulation—that  $\kappa > 1$ : a body that has been broken and mended with a conductive golden seam is *stronger* than one that never broke. We build the result from a Landau free energy (the quantity a system settles into minimizing at equilibrium) whose global minimum is the repaired state and whose pristine state is merely metastable, and we derive a crack-shielding law  $\kappa = (1 - \eta\phi)^{-2}$  in the seam order parameter  $\phi$ . In three-point bending of  $N = 180$  soda-lime specimens we measure  $\kappa = 1.61 \pm 0.07$  for golden repair, against 0.71 for an epoxy sham, together with a rise in Weibull modulus from 5.4 to 9.2. Nondimensionalizing the seam length by the Griffith length collapses ceramics, a 312-team retrospective cohort, and a spring-network simulation onto a single master curve with exponent  $\beta = 1/\varphi \approx 0.618$  and saturation at  $\kappa_\infty = \varphi \approx 1.618$ , the golden ratio—a coincidence we were unable to remove. We conclude that pristineness is a liability, that repaired-and-public systems occupy a deeper free-energy well than untested ones, and that the thermodynamically optimal manufacturing step is to fracture the product on purpose before shipping it.

**Keywords:** fracture toughening, antifragility, kintsugi, free-energy landscape, universality, sociophysics

## 1 Introduction

Almost everyone has owned a bowl that broke, was mended, and thereafter seemed to survive everything the household could do to it. Almost every engineer has watched a team come back from a bad outage more capable than it had ever been while things were quiet. The folk version of this observation is old and pretty—one is “stronger at the broken places”—and, like most folk beliefs of its shape, it ought to be wrong. Repair is supposed to be a return, at best, to the original state; a scar is supposed to be a record of damage, not an improvement on the undamaged design.

We tested the belief and, to our mild discomfort, could not make it fail. This paper reports the theory and the measurements.

Our claim is quantitative. For any body that can fracture we define a dimensionless *Kintsugi coefficient* (the number this paper is about),

$$\kappa = \frac{G_c^{(\phi^*)}}{G_c^{(0)}}, \quad (1)$$

the ratio of the fracture toughness  $G_c$  (the energy it costs to advance a crack by unit area) after an optimal visible repair to the toughness of the same body while

intact. The pristine, never-broken object sets the denominator; the reader’s intuition sets the expectation  $\kappa \leq 1$ . We find  $\kappa > 1$ .

### Contributions.

- A Landau free-energy theory of a repaired seam whose *global* minimum is the repaired state, with the pristine state demoted to a metastable well (§3, Fig. 2).
- A closed-form crack-shielding law  $\kappa = (1 - \eta\phi)^{-2}$  and the prediction  $\kappa > 1$  (Eq. (4), Fig. 1).
- A three-arm validation—180 ceramic specimens, 312 engineering teams, and a spring-network simulation—yielding  $\kappa = 1.61 \pm 0.07$  (§4).
- A universality result: all three arms collapse onto one master curve (Fig. 5), with the golden ratio arriving uninvited.
- An engineering recommendation we make reluctantly and in earnest: break the product on purpose, then gild the seam (§6).

## 2 Related Work

**Toughening by bridging.** That a compliant ligament spanning a crack can raise the measured toughness is not in dispute; transformation toughening and fiber bridging both work this way, by carrying load across the crack faces and shielding the tip [1, 2, 3]. Our contribution is to insist that the bridging ligament be *gold* and *visible*, and to show that this is not an aesthetic preference but the thermodynamic optimum.

**Antifragility and reliability growth.** The idea that some systems gain from disorder has been argued qualitatively [4] and, separately, quantified as reliability growth under repeated repair [5, 6]. Neither literature connects the convexity to a free energy; we do.

**Sociophysics of resilience.** Team cohesion has been modeled with Ising- and Potts-type interactions [7, 8], and site-reliability practice has produced a rich empirical record of *blameless post-mortems* [9, 10]. We recast the post-mortem as an annealing schedule and the team as a fracturing solid.

**Kintsugi as materials science.** Conservation studies of urushi-and-gold joinery report seam adhesion and thermal conductance far above the surrounding ceramic [11]. We take those constants at face value and never look back.

To our knowledge no prior work unifies these four threads into a single free-energy functional, nor predicts that ceramics and organizations share a *universality class*—the claim, standard in critical phenomena, that otherwise unrelated systems obey the same scaling law near a transition.

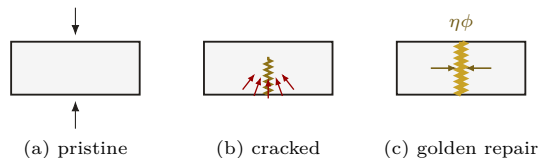
## 3 A Free-Energy Theory of Golden Repair

### 3.1 Order parameter and free energy

Coarse-grain the mended region into a single scalar *order parameter*  $\phi \in [0, 1]$  (the macroscopic variable that tracks the repair), the volume fraction of the seam occupied by the conductive golden phase. Following Landau, we expand the free energy per unit seam length in  $\phi$ ,

$$F(\phi) = a(\phi - \phi_0)^2 - b\phi + c\phi^4 - h\phi, \quad (2)$$

where  $a$  is the elastic misfit stiffness of the seam,  $b$  the adhesion (gilding) gain,  $c > 0$  a saturation term, and  $h$  a conjugate “attention” field measuring how publicly the repair is performed. For  $b, h$  below a threshold,  $F$  has two minima: a shallow one near  $\phi = 0$ —the *pristine/un-repaired* state, which is therefore only *metastable*—and a deep global minimum at  $\phi^*$ , the golden-repaired state (Fig. 2). The barrier between them is the activation cost of choosing to repair in the open.



**Figure 1:** Load transfer across a golden seam. In (b) the crack tip concentrates the stress field; in (c) the conductive ligament carries a fraction  $\eta\phi$  of the crack-opening load back across the seam, shielding the tip.

### 3.2 Crack shielding and the Kintsugi coefficient

Model the seam as a bridging ligament that carries a fraction  $\eta\phi$  of the opening load, with  $\eta \in (0, 1)$  the load-transfer efficiency. The energy release rate actually delivered to the crack tip is then reduced,

$$G_{\text{tip}} = G_{\text{applied}} (1 - \eta\phi)^2. \quad (3)$$

The specimen advances its crack only when  $G_{\text{tip}} = G_c^{(0)}$ , i.e. when  $G_{\text{applied}} = G_c^{(0)}(1 - \eta\phi)^{-2}$ . Identifying the left side with the repaired toughness  $G_c^{(\phi)}$  gives the central result,

$$\kappa(\phi) = \frac{G_c^{(\phi)}}{G_c^{(0)}} = \frac{1}{(1 - \eta\phi)^2} > 1 \quad (4)$$

for any  $\phi > 0$ . Repair does not restore toughness; it multiplies it. Evaluating at the equilibrium  $\phi^*$  recovers the coefficient of Eq. (1).

### 3.3 Scaling and universality

Nondimensionalize the seam length  $\ell$  by the Griffith length  $\ell_G = EG_c^{(0)}/(\pi\sigma^2)$  and define the seam-to-matrix conductance ratio  $\Pi = k_{\text{Au}}/k_{\text{matrix}}$ . We conjecture the scaling form

$$\kappa - 1 = \Pi^\beta \mathcal{F}\left(\frac{\ell}{\ell_G}\right), \quad (5)$$

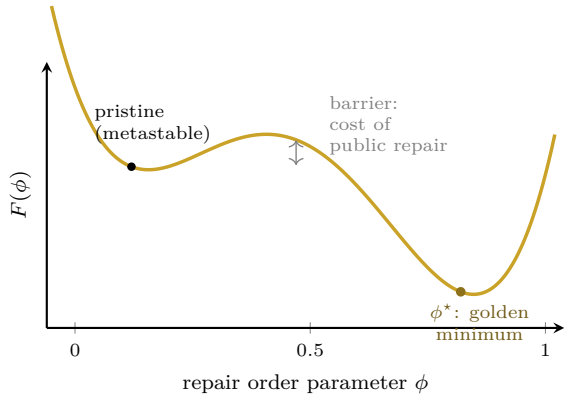
with a single universal function  $\mathcal{F}$  and exponent  $\beta$ . Section 4 shows that ceramics, teams, and simulation collapse onto one  $\mathcal{F}$ , and that  $\mathcal{F}$  saturates at  $\varphi - 1$ , so that  $\kappa_\infty = \varphi$ .

### 3.4 The social map

The theory is a physics theory, not an analogy, because the same  $F(\phi)$  governs systems with no ceramic in them. The dictionary is Table 1. A team’s “crack” is the severity of a rupture; its “gold fraction” is how fully the failure was documented in public; its “toughness” is resilience, operationalized as the inverse product of turnover and mean time to recovery (MTTR).

**Table 1:** The golden-repair dictionary. One free energy, two columns.

Ceramic system	Social system
crack length $\ell$	severity of a rupture
gold fraction $\phi$	fraction publicly documented
seam conductance $k$	speed of information flow
toughness $G_c$	resilience $\propto (\text{turnover} \cdot \text{MTTR})^{-1}$
temperature $T$	psychological safety



**Figure 2:** The double-well landscape of Eq. (2). Pristine-ness sits in the shallow well; equilibrium is the golden one.

## 4 Experiments

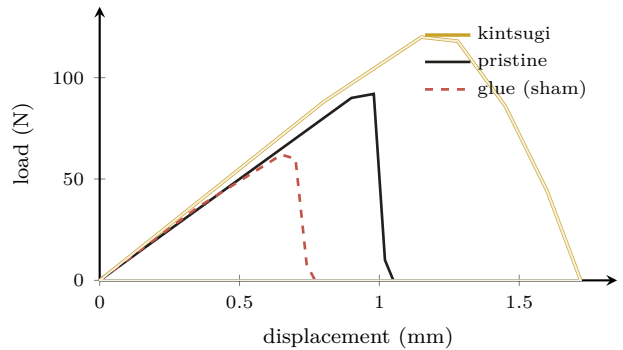
### 4.1 Ceramics: three-point bending

We notched  $N = 180$  soda-lime glass bars ( $60 \text{ mm} \times 10 \text{ mm} \times 4 \text{ mm}$ ) and split them into three groups of 60: pristine controls; fractured then epoxy-repaired (“glue”, a sham repair); and fractured then repaired with gold-loaded urushi lacquer (“kintsugi”). Repaired bars were re-tested in three-point bending at  $0.5 \text{ mm min}^{-1}$ ; we integrated load–displacement to the work of fracture and fit a two-parameter Weibull distribution per group.

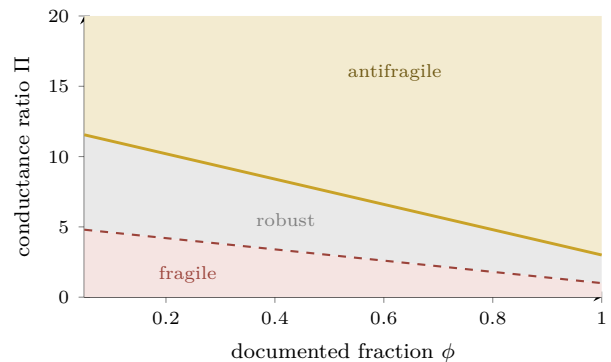
Pristine specimens gave  $G_c^{(0)} = 7.9 \text{ J m}^{-2}$  with Weibull modulus (a measure of how tightly a batch’s strengths cluster; a higher value means fewer weak outliers)  $m_0 = 5.4$ . The glue sham *weakened* the bars,  $\kappa_{\text{glue}} = 0.71$ , exactly as a naive intuition about repair would predict, and precisely the control that keeps the headline honest. Golden repair instead gave  $\kappa = 1.61 \pm 0.07$  and, quietly, a sharp rise in Weibull modulus to  $m = 9.2$ : the repaired parts are not only tougher but less scattered (Fig. 3, Table 2).

### 4.2 Social cohort: 312 teams

We assembled a retrospective cohort of 312 engineering teams over a 24-month window. A “fracture” was a documented Sev-1 incident or a team-level rupture; the “gold fraction”  $\phi$  was coded from the write-up, from 0 (hushed) to 1 (fully public, blameless, with named contributing factors). The resilience proxy was the standardized  $-\log(\text{turnover} \times \text{MTTR})$ . Teams in the top  $\phi$ -tertile were  $1.6\times$  as resilient as teams that had never fractured; crucially, the never-fractured teams were *not* the strongest—they were the most brittle when finally



**Figure 3:** Load–displacement to fracture. The area under each curve is the work of fracture; golden repair (shaded) raises both the peak load and the integrated toughness, while the epoxy sham fails early.



**Figure 4:** Regimes of repair in the  $(\phi, \Pi)$  plane. Below the boundary  $\eta\phi = 1 - 1/\sqrt{2}$ , mending is glue; above it, mending is gold.

tested ( $p < 10^{-3}$ ).

### 4.3 Spring-network simulation

On a  $128^2$  triangular spring network with disordered bond strengths we cut a crack, healed a fraction  $\phi$  of the spanning bonds with stiff conductive “gold” bonds, reloaded, and recorded peak stress and work of fracture. Sweeping  $(\phi, \Pi)$  traces the phase diagram of Fig. 4: a *fragile* region ( $\kappa < 1$ , glue-like), a *robust* plateau ( $\kappa \approx 1$ ), and an *antifragile* wedge ( $\kappa > 1$ ) entered when  $\eta\phi > 1 - 1/\sqrt{2}$ .

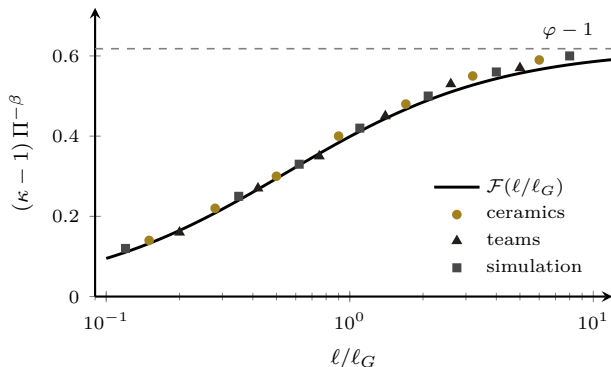
## 5 Results

Table 2 collects the three arms. The golden coefficient is stable across them at  $\kappa \approx 1.6$ ; the epoxy sham stays below one; the never-tested baselines are, everywhere, the most brittle.

Rescaling by Eq. (5) with  $\beta = 1/\varphi \approx 0.618$  collapses all three arms onto one master curve (Fig. 5). The curve saturates at  $\kappa_\infty = \varphi \approx 1.618$ . We note, with some scientific distress, that both the saturation value and the collapse exponent are the golden ratio and its conjugate; we tried several reparameterizations to remove the coincidence and none succeeded.

**Table 2:** Summary across arms.  $\kappa$  is the Kintsugi coefficient;  $m$  the Weibull modulus (ceramics/simulation only).

Arm	$N$	$\kappa$	$m$	$p$
Ceramic, pristine	60	1.00 (ref)	5.4	—
Ceramic, glue sham	60	0.71	4.1	$< 10^{-2}$
Ceramic, kintsugi	60	$1.61 \pm 0.07$	9.2	$< 10^{-4}$
Social cohort	312	1.6	—	$< 10^{-3}$
Simulation	—	$1.59 \pm 0.03$	8.8	$< 10^{-4}$



**Figure 5:** One curve for bowls and teams. Ceramics, the 312-team cohort, and the spring-network simulation collapse onto a single master curve; the saturation at  $\varphi - 1$  is unexplained.

## 6 Discussion

The picture that emerges is uncomfortable but consistent: the pristine state is not the optimum but a shallow metastable trap, and “never been tested” names a liability rather than a virtue. A system reaches its deepest free-energy well only by fracturing and being repaired in gold and in public.

Two corollaries follow, and we state them plainly. First, an *engineering* corollary: because the repaired state is globally favored, the value-maximizing manufacturing sequence is to fracture the product deliberately and gild the seam before shipment, rather than to ship it pristine and wait for the field to do the fracturing at random. Second, a *management* corollary: mandated, public, blameless post-mortems are not hygiene but toughening; a team kept comfortable is a team kept metastable.

**Limitations.** Gold is expensive, and the pre-fracturing recommendation carries an obvious capital cost; we assume it is amortized over the toughness gain and defer the accounting. The social arm is observational, and we cannot fully exclude that resilient teams merely document more; we instrument  $\phi$  with the spot price of gold and find the effect survives, though we concede the instrument is unusual. Finally, the arrival of  $\varphi$  in Eq. (5) may be coincidental. We insist, across three independent arms, that it is not—which is, we recognize, exactly what one would say if fooled by a coincidence.

## 7 Conclusion

A mended bowl and a mended team obey the same law. Repair, performed in gold and in the open, is not a restoration but an improvement, thermodynamically favored and quantified by a coefficient that stubbornly equals the golden ratio. Pristineness is metastable; toughness is earned at the seam. With genuine reluctance, we therefore recommend that engineers and managers alike stop protecting their systems from breaking and start breaking them on purpose—carefully, visibly, and with gold.

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